

## **MULTI-TUBE SOLAR COLLECTOR STRUCTURE**

### **FIELD OF THE INVENTION**

5 This invention relates to a solar collector structure that employs a plurality of absorber tubes that are arranged to be illuminated by solar radiation from a reflector field and to transfer absorbed energy to a heat exchange fluid that is, in use of the structure, carried by the tubes. The invention has been developed in the context of a so-called compact  
10 linear Fresnel reflector (CLFR) system and is hereinafter described in relation to such a system. However, it will be understood that the invention may have broader application.

### **BACKGROUND OF THE INVENTION**

15 Prior art solar collector structures of the type with which the present invention might be compared may be categorised generally as falling within two groups; a first group that employs effectively a single absorber tube that extends along the focal line of a non-inverted trough-type reflector and a second group that employs a single absorber  
20 tube that extends along the focal line of an inverted trough-type reflector. Collector systems of the first group suffer the disadvantages that the absorber tube collects incident solar energy from one only reflector element and requires complex mounting and fluid coupling arrangements. Collector systems of the second group largely avoid the  
25 disadvantages of the first group but suffer the disadvantage of losses occasioned by the need for multiple reflections, firstly from ground-mounted reflectors and then from the inverted trough reflectors.  
Moreover, collector systems of the second group (if not both groups)  
suffer a relatively high emissivity-to-absorptance ratio as a  
30 consequence, in part, of the surface area-to-aperture ratio attributable to the relatively large diameter tube required of a single-tube collector system. Furthermore, as a secondary issue, collector systems of both

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the first and second groups suffer loss of operating efficiency due to movement of unconfined heated air from the interior of the trough-like reflectors. Still further, as a tertiary issue, to the extent that the collector systems of the first and second groups employ a single  
5 absorber tube, those collector systems are not capable of providing for a variable absorption aperture.

### **SUMMARY OF THE INVENTION**

The present invention provides a collector structure that is arranged to  
10 be located at a level above a field of reflectors and to receive solar radiation reflected from reflectors within the field. The collector structure comprises an inverted trough and, located within the trough, a plurality of longitudinally extending absorber tubes that, in use, are arranged to carry a heat exchange fluid. The absorber tubes are  
15 supported side-by-side within the trough and each absorber tube has a diameter that is small relative to the aperture of the trough.

The ratio of each absorber tube diameter to the trough aperture dimension may, for example, be in the range of 0.01:1.00 to 0.10:1.00  
20 and typically may be of the order of 0.03:1.00. With this arrangement the plurality of tubes will, in the limit, effectively simulate a flat plate absorber.

The expressions "aperture of the trough" and "trough aperture" are both  
25 intended to be understood as defining, effectively, the opening of the trough through which incident radiation may pass to impinge on the absorber tubes.

A plurality of the collector structures as above defined may be  
30 connected together co-linearly to form a row of the structures and, in such case, each of the absorber tubes will extend along the full row, either as a single length of tubing or as conjoined lengths of tubing.

**OPTIONAL FEATURES OF THE INVENTION**

The absorber tubes may be constituted by metal tubes and each tube may, if required, be coated over at least a portion of its surface with a solar absorptive coating. In an alternative arrangement, each absorber

5      tube may comprise a glass or metal tubular component that is coated with a solar selective surface coating and a surrounding glass tubular component, with the space between the two tubular components being evacuated.

10     The inverted trough may (but need not necessarily) be located in spaced relationship below a longitudinally extending roof and, in such case, an insulating material may be located in the space between the trough and the roof.

15     A window that is substantially transparent to solar radiation may be employed to close (the aperture of) the trough and, in so doing, create a heat confining cavity within the trough. The window may be formed from a rigid material such as glass or it may, for example, be formed from a flexible plastics sheet material that is connected to marginal side

20    wall portions of the trough. In this latter case the cavity may be pressurised to an extent sufficient to inflate the window in a direction away from the absorber tubes.

The heat exchange fluid may in use of the collector structure be

25    controlled to flow in parallel, unidirectional streams through the plurality of absorber tubes. Alternatively, means may be provided for selectively varying the channelling of the heat exchange fluid into and through the plurality of absorber tubes whereby the absorption aperture of the collector structure may, in use, effectively be varied.

30    The invention will be more fully understood from the following description of an exemplary embodiment of the solar collector structure.

The description is provided, by way of example, with reference to the accompanying drawings.

#### **BRIEF DESCRIPTION OF THE DRAWINGS**

5 In the drawings-

Figure 1 shows a largely diagrammatic representation of a CLFR system that comprises a field of ground mounted reflectors that are arrayed in rows and collector systems that are constituted by rows of aligned collector structures;

10 Figure 2 illustrates schematically the reflection of solar radiation from four reflectors to two collector systems within the CLFR system;

Figure 3 shows an aerial view of a portion of a field of reflectors and a single collector structure positioned adjacent one edge of the field;

15 Figure 4 shows a perspective view (from above) of a terminal end of a collector structure of the type shown in Figure 3;

Figure 5 shows a sectional end view of the collector structure of Figure 4;

Figure 6 shows a portion of the collector structure which is encircled by circle A in Figure 5;

20 Figure 7 shows a portion of the collector structure which is encircled by circle B in Figure 5;

Figure 8 shows diagrammatically a fluid flow control arrangement for a collector system that comprises a row of four interconnected collector structures; and

25 Figures 9A, 9B and 9C show alternative fluid channelling arrangements that provide for different effective absorption apertures.

#### **DETAILED DESCRIPTION OF THE INVENTION**

As shown in Figures 1 to 3, the CLFR system comprises a field of

30 ground mounted reflectors 10 that are arrayed in rows 11 and further comprises parallel collector systems 12, each of which is constituted by aligned collector structures 13. A complete CLFR system might occupy

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a ground area within the range  $5 \times 10^1 \text{ m}^2$  to  $25 \times 10^6 \text{ m}^2$  and the system as illustrated in Figure 1 may be considered as a portion only of a larger CLFR system.

5 The reflectors 10 may be of the type described in co-pending International Patent Applications numbered PCT/AU2004/000883 and PCT/AU2004/000884, filed 01 July 2004 by the present Applicant, and the disclosures of these Patent Applications are incorporated herein by reference.

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The reflectors 10 are driven collectively or regionally, as rows or individually, to track movement of the sun (relative to the earth) and they are orientated to reflect incident radiation to respective ones of the collector systems 12, as shown schematically and by way of example in

15 Figure 2. Also, some or all of the reflectors 10 may be driven so as to reorientate, when required, to change the direction of reflected radiation from one collector system 12 to another.

20 In the system as illustrated in Figure 1, and as may typically be the case, each collector system 12 receives reflected radiation from twelve rows of reflectors 10. Thus, each collector system 12 receives reflected radiation from six rows at one side of the collector system and from six rows at the other side, although (as indicated in Figure 2) the reflecting rows that are associated with any one receiving collector system need 25 not necessarily be located immediately adjacent that receiving collector system.

30 Each row 11 of reflectors 10 and, hence, each collector system 12 might typically have an overall length of 300 metres, and the parallel collector systems 12 might typically be spaced apart by 30 to 35 metres. The collector systems 12 are supported at a height of approximately 11 metres by stanchions 14 which are stayed by ground-anchored guy

wires 15, although other similar support arrangements might be employed.

As indicated previously, each of the collector systems 12 comprises a plurality of collector structures 13 that are connected together co-linearly to form a row of the structures. Each of the collector structures might typically have a length of the order of 12 metres and an overall width of the order of 1.4 metres.

Each collector structure 13 comprises an inverted trough 16 which might typically be formed from stainless steel sheeting and which, as best seen in Figure 5, has a longitudinally extending channel portion 17 and flared side walls 18 that, at their margins, define an aperture of the inverted trough. The trough 16 is supported and provided with structural integrity by side rails 19 and transverse bridging members 20, and the trough is surmounted by a corrugated steel roof 21 that is carried by arched structural members 22.

The void between the trough 16 and the roof 21 is filled with a thermal insulating material 23, typically a glass wool material, and desirably with an insulating material that is clad with a reflective metal layer. The function of the insulating material and the reflective metal layer is to inhibit upward conduction and radiation of heat from within the trough.

A longitudinally extending window 24 is provided to interconnect the side walls 18 of the trough. The window is formed from a sheet of material that is substantially transparent to solar radiation and it functions to define a closed (heat retaining) longitudinally extending cavity 25 within the trough.

The window 24 may be formed from glass but it desirably is formed from a transparent heat resistant plastics material having a thickness

of the order of  $60 \times 10^{-6}$  m. As shown in Figure 7, side margins of the window may be welded to a wire or other heat resistant rope core 26 and the window may be held in position by slideably locating the cored side margins in fluted side connectors 27.

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Figure 4 shows a collector structure 13 that is intended to be located at a terminal end of a row 12 of the collector structures, and it is provided with an end wall 28 to which is mounted a motor driven blower 29. The blower is provided in use to maintain a positive air pressure within the cavity 25 (relative to the ambient atmospheric pressure) and so to inflate the window in a direction away from absorber tubes 30 within the inverted trough 16.

In the collector structure as illustrated, sixteen longitudinally extending stainless steel absorber tubes 30 are provided for carrying heat exchange fluid (typically water or, following heat absorption, water-steam or steam). However, the actual number of absorber tubes may be varied to suit specific system requirements, provided that each absorber tube has a diameter that is small relative to the dimension of the trough aperture between the side walls 19 of the trough, and the collector system might typically have between ten and thirty absorber tubes 30 supported side-by-side within the trough.

The actual ratio of the absorber tube diameter to the trough aperture dimension may be varied to meet system requirements but, in order to indicate an order of magnitude of the ratio, it might typically be within the range 0.01:1.00 to 0.10:1.00. Each absorber tube 30 might have an outside diameter of 33 mm. and, with an aperture dimension of, for example, 1100mm, the ratio of the absorber tube diameter to the aperture dimension will be 0.03:1.00.

As indicated previously, with the above described arrangement the plurality of absorber tubes 30 will, in the limit, effectively simulate a flat

plate absorber, as compared with a single-tube collector in a concentrating trough. This provides for increased operating efficiency, in terms of a reduced level of heat emission from the upper, non-illuminated circumferential portion of the absorber tubes. Moreover, by 5 positioning the absorber tubes in the inverted trough in the manner described, the underside portion only of each of the absorber tubes is illuminated with incident radiation, this providing for efficient heat absorption in absorber tubes that carry steam above water.

10 As illustrated in Figure 6, the absorber tubes 30 are freely supported by a series of parallel support tubes 31 which extend orthogonally between side walls 32 of the channel portion 17 of the inverted trough, and the support tubes 31 are carried for rotational movement by spigots 33. This arrangement accommodates expansion of the absorber tubes and 15 relative expansion of the individual tubes. Disk-shaped spacers 34 are carried by the support tubes 31 and serve to maintain the absorber tubes 30 in spaced relationship.

20 Each of the absorber tubes 30 is coated, along its length and around a (lower) portion of its circumference that is exposed to incident solar radiation, with a solar absorptive coating. The coating may comprise a solar selective surface coating that remains stable under high temperature conditions in ambient air or it may comprise a black paint that is stable in air under high-temperature conditions.

25 Figure 8 of the drawings shows diagrammatically a flow control arrangement for controlling flow of heat exchange fluid into and through four in-line collector structures 13 of a collector system. As illustrated, each of the fluid lines 30A, B, C and D is representative of 30 four of the absorber tubes 30 as shown in Figure 5.

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Under the controlled condition illustrated in Figure 8, in-flowing heat exchange fluid is first directed along forward line 30A, along return line 30B, along forward line 30C and finally along and from return line 30D. This results in fluid at a lower temperature being directed through  
5 tubes that are located along the margins of the inverted trough and a consequential emission reduction when radiation is concentrated over the central region of the inverted trough. An electrically actuated control device 35 is provided to enable selective control over the channelling of the heat exchange fluid.

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Alternative fluid flow conditions may be established to meet load demands and/or prevailing ambient conditions, and provision may effectively be made for a variable aperture collector structure by closing selected ones of the absorber tubes. Thus, variation of the effective  
15 absorption aperture of each collector structure and, hence, of a complete collector system may be achieved by controlling the channelling of the heat exchange fluid in the alternative manners shown in Figures 9A to 9C.

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It is to be understood that the embodiment of the invention as described with reference to the drawings is presented solely as an example of one possible form of the invention. Thus, variations and modifications may be made in the embodiment of the invention as described without departing from the spirit and scope of the invention  
25 as defined in the appended claims.

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